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# **Ranging detection algorithm for indoor UWB channels and research activities relating to a UWB-RFID localization system**

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# Contents

- Introduction to UWB-RFID localization
- Indoor UWB channel measurements
- Ranging detection algorithm
- Results on one way ranging accuracy
- Active UWB-RFID localization based on TDOA

# Scalable UWB-RFID Positioning System

## Motivation

An ultra-wideband (UWB) enabled radio frequency identification (RFID) system

- scalable real time identification, localization, positioning and tracking of objects/nodes.
- scalability to thousands of nodes over area size of hundreds of meters
- applications such as logistics and environmental monitoring and protection
- positioning capability at sub-meter level using low power (<10mW) active tags and (<100 uW) passive tags.

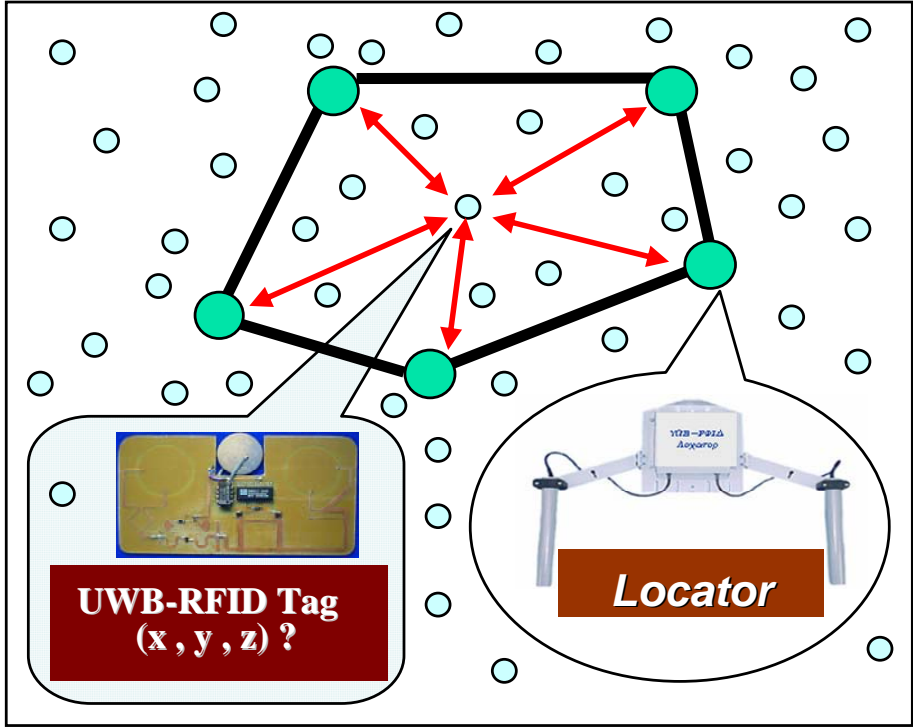


Figure 1: Scalable UWB-RFID Localization System

## Innovative Ideas

Our innovative ideas are centered on UWB enabled backscatter RFID system architecture. For example, passive tags mounted on the walls will help to guide visually handicapped person to navigate in his home or a shopper to localize his position with respect to the goods that he wish to purchase



# Indoor UWB channel measurements

## Measurement Campaign Objectives

- Obtain a database of UWB channel profiles in various indoor environments.
- Test UWB ranging accuracy in indoor environment with FCC PSD mask compliance UWB signal and Model the ranging error statistically.
- Analyze the UWB ranging performance in indoor environment and use the analysis to facilitate the ranging parameters setting in both LOS and NLOS cases.

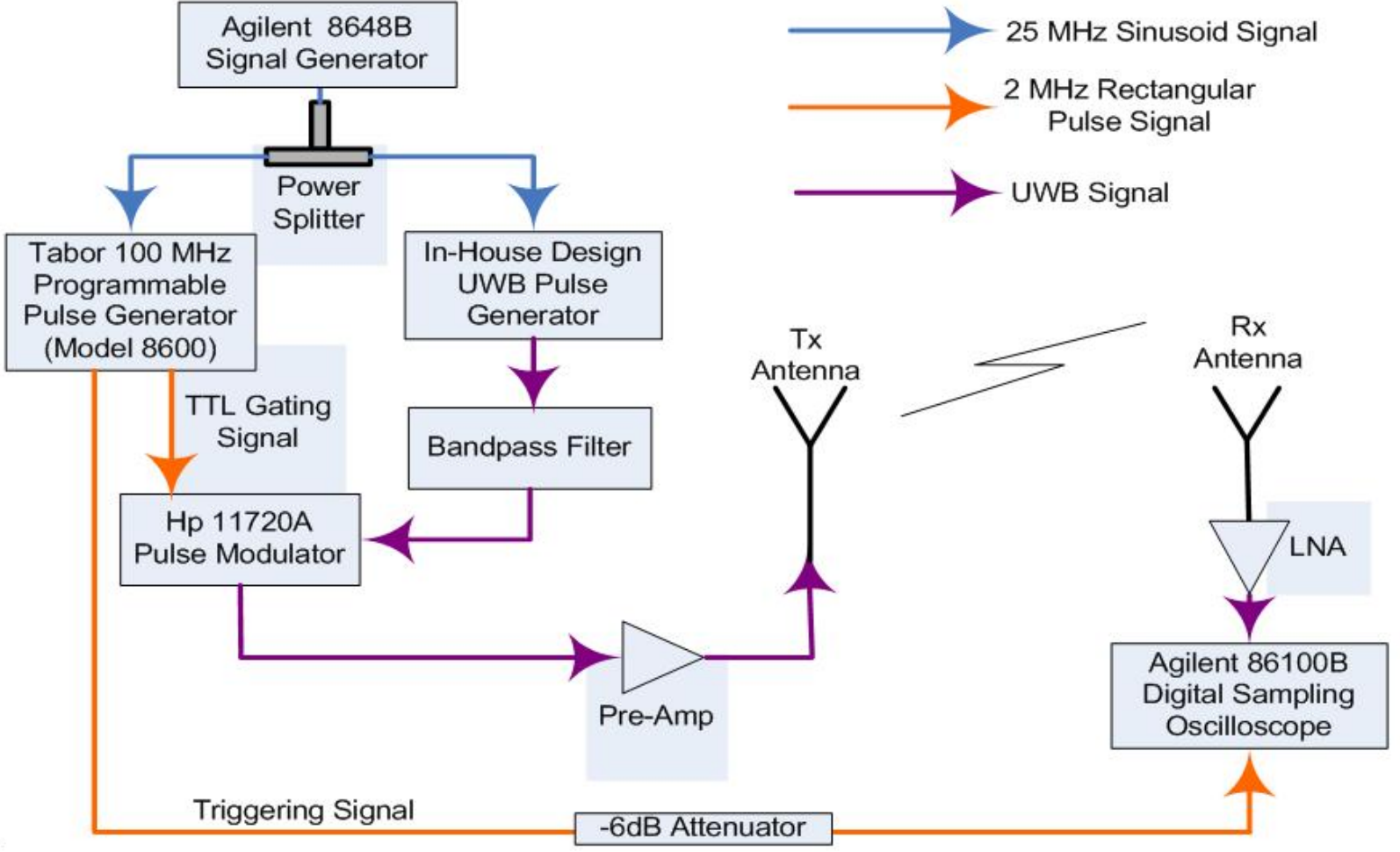


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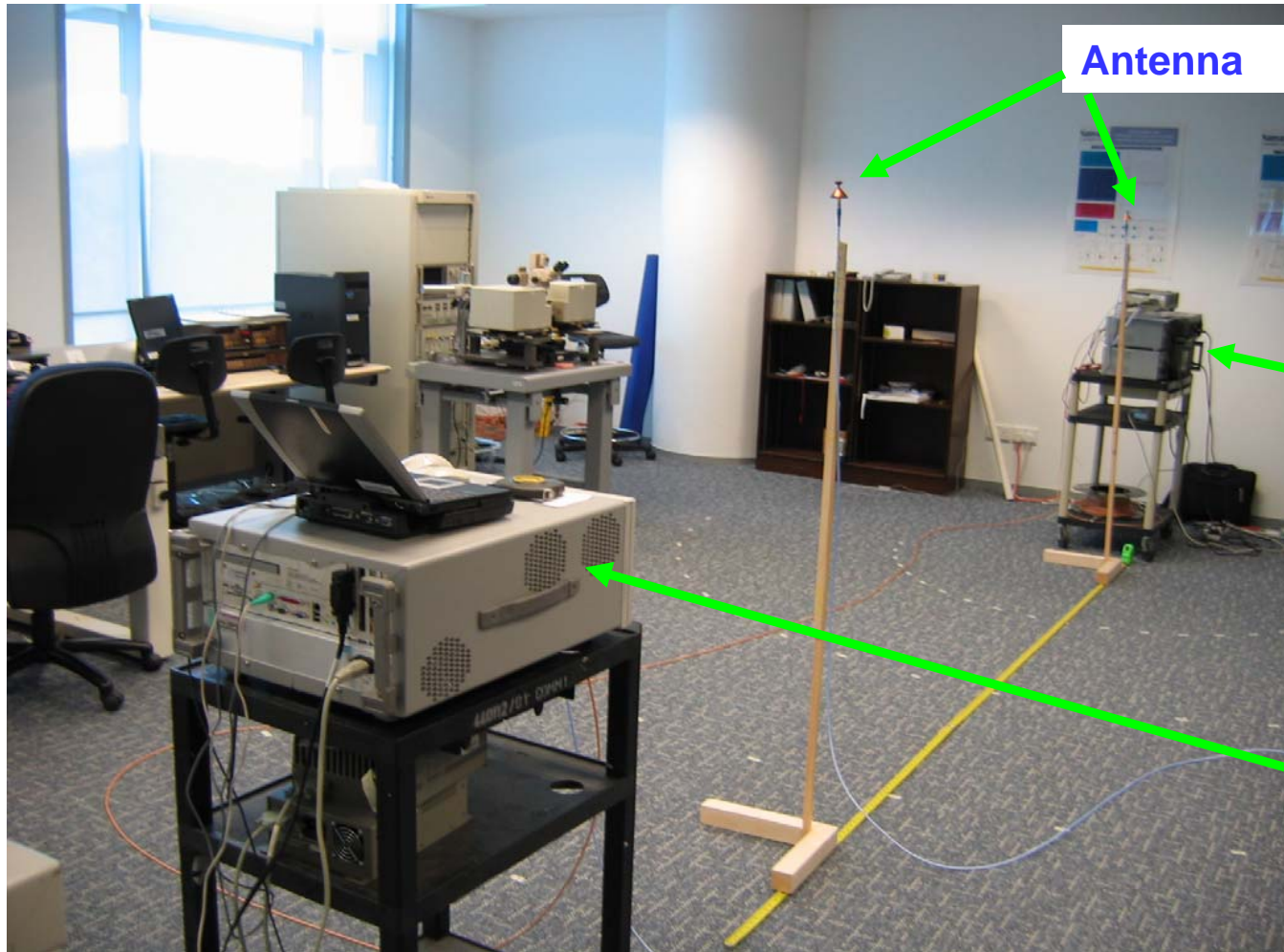
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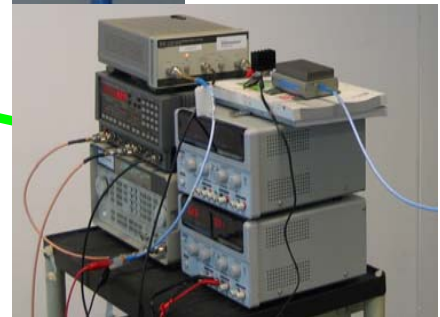
# Measurement System Setup



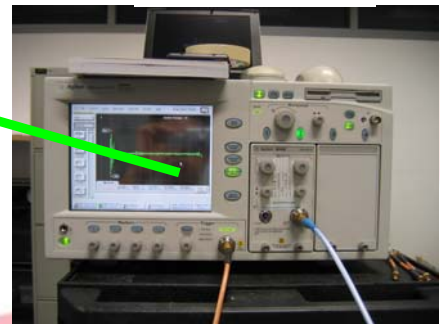
# Measurement Setup



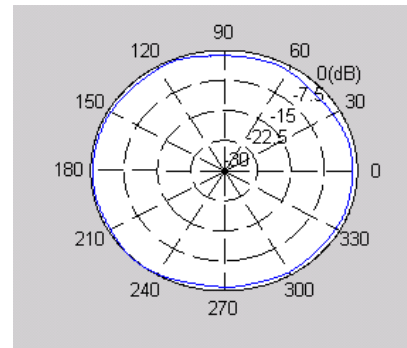
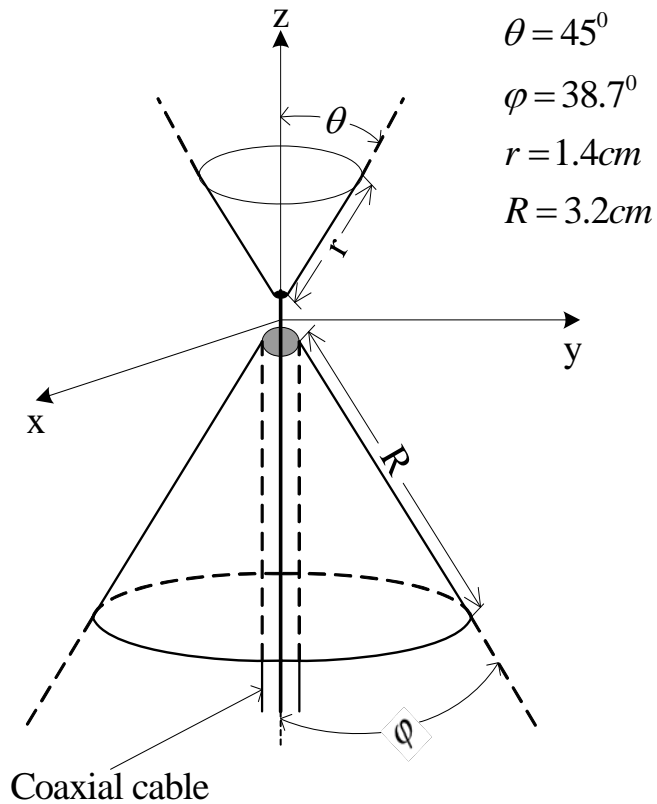
Tx Setup



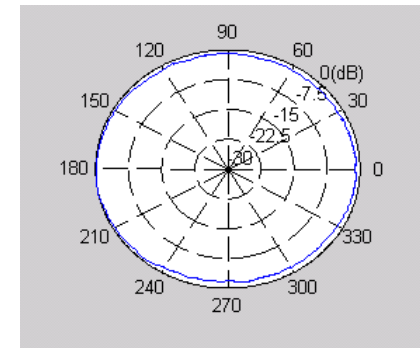
Rx Setup



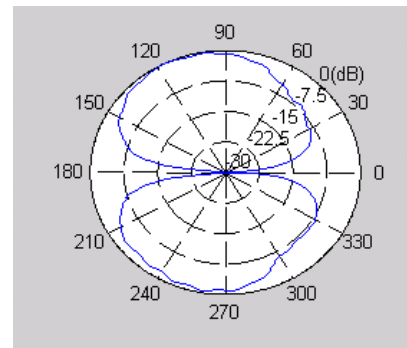
# Bi-conical Antenna Pattern



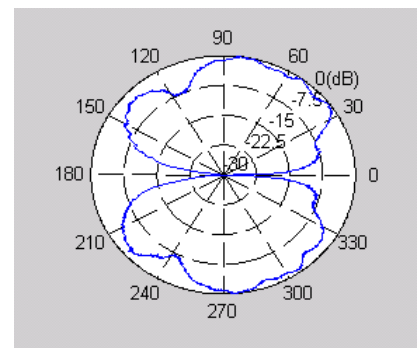
**3.1GHz Azimuth Plane**



**10.6 GHz Azimuth Plane**

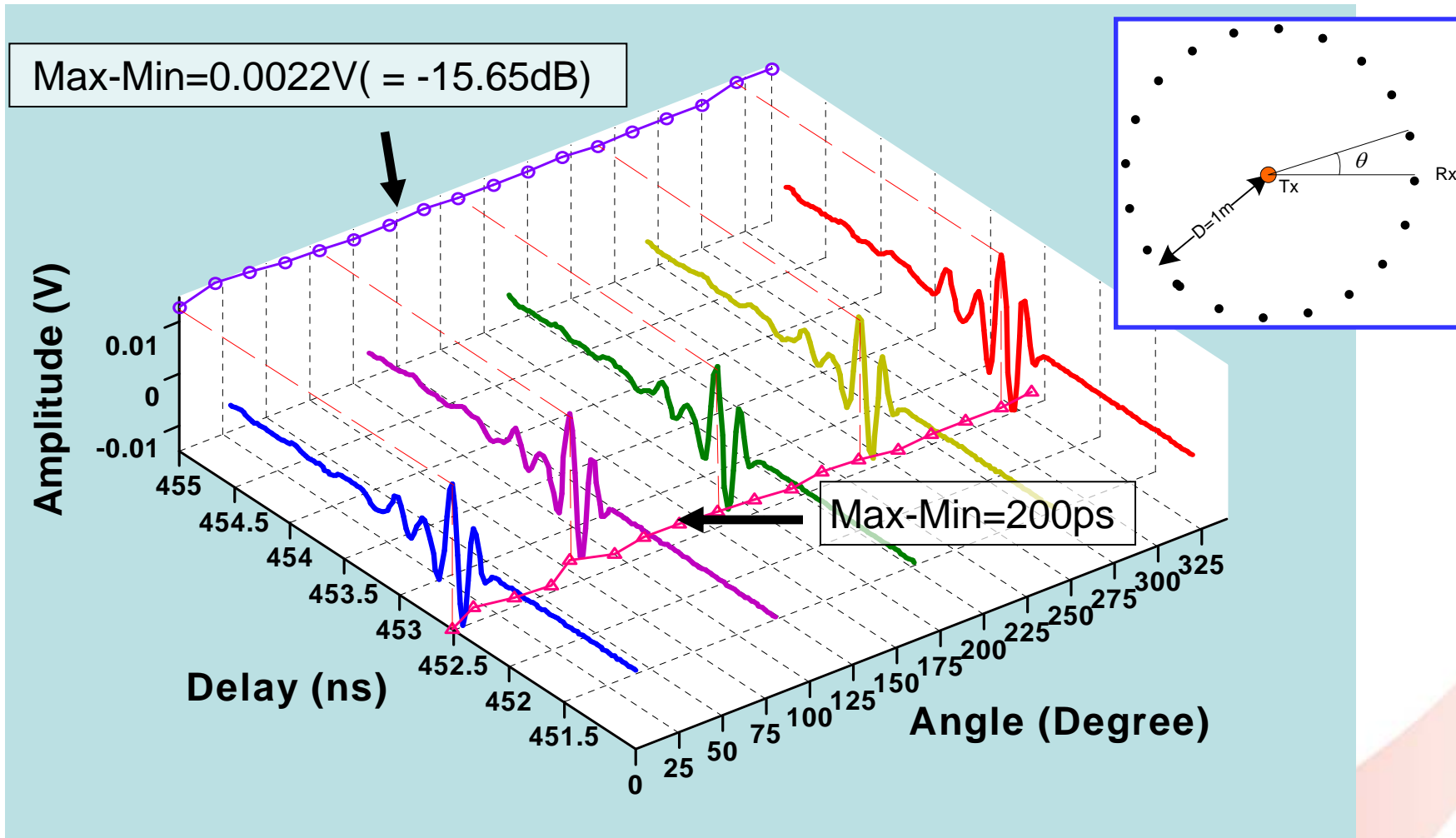


**3.1GHz Elevation Plane**



**10.6 GHz Elevation Plane**

# Test the Omni-directional properties of measurement setup





# Measurement Environment

Indoor Office



Laboratory Room



Open Hall



Corridor



# Campaign Summary

| Environment   | Sample Points | Sample Spacing | Maximum Distance | LOS or NLOS   |
|---------------|---------------|----------------|------------------|---------------|
| Indoor Office | 1257          | 0.2m           | 26m              | LOS and NLOS* |
| Lab           | 271           | 0.2m           | 5m               | LOS           |
| Open Hall     | 61            | 0.5m           | 30m              | LOS           |
| Corridor      | 31            | 1m             | 30m              | LOS           |
| Total         | 1620          |                |                  |               |

\* LOS – Line of Sight NLOS – Non Line of Sight



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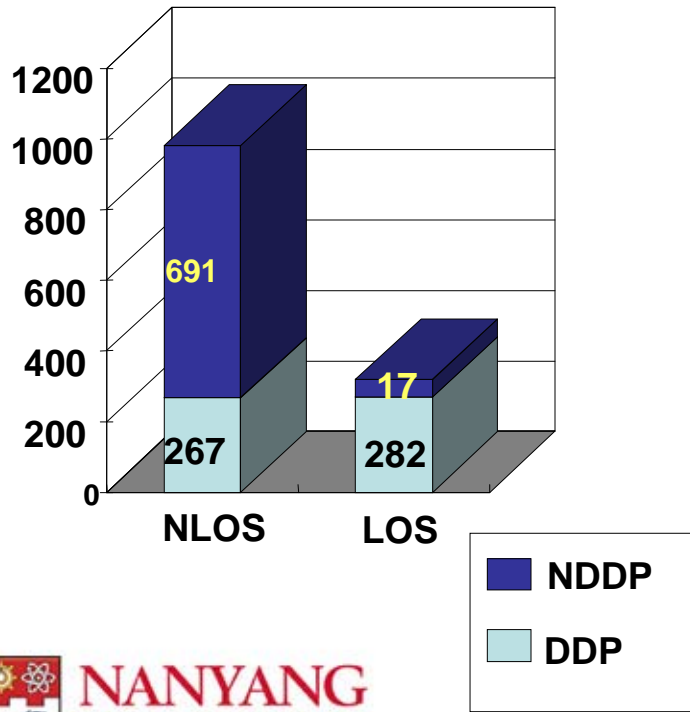
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# Indoor Office Layout with Measurement Routes

- 1257 measurement points in indoor environment
- 0.2 meter spacing
- Maximum distance is 26 meters

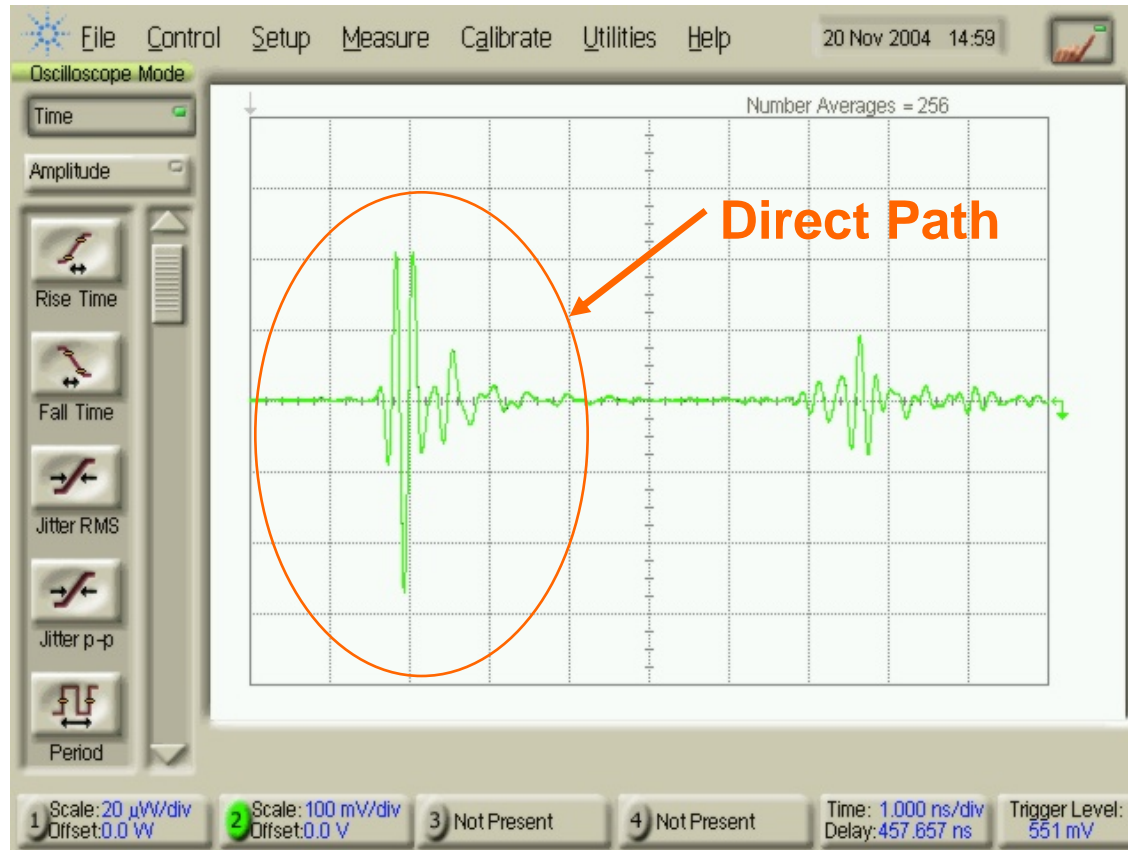


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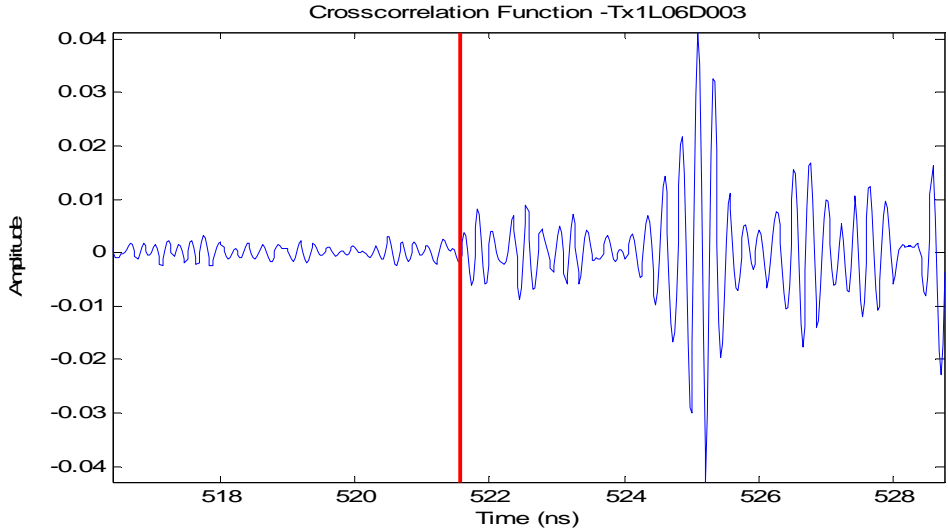
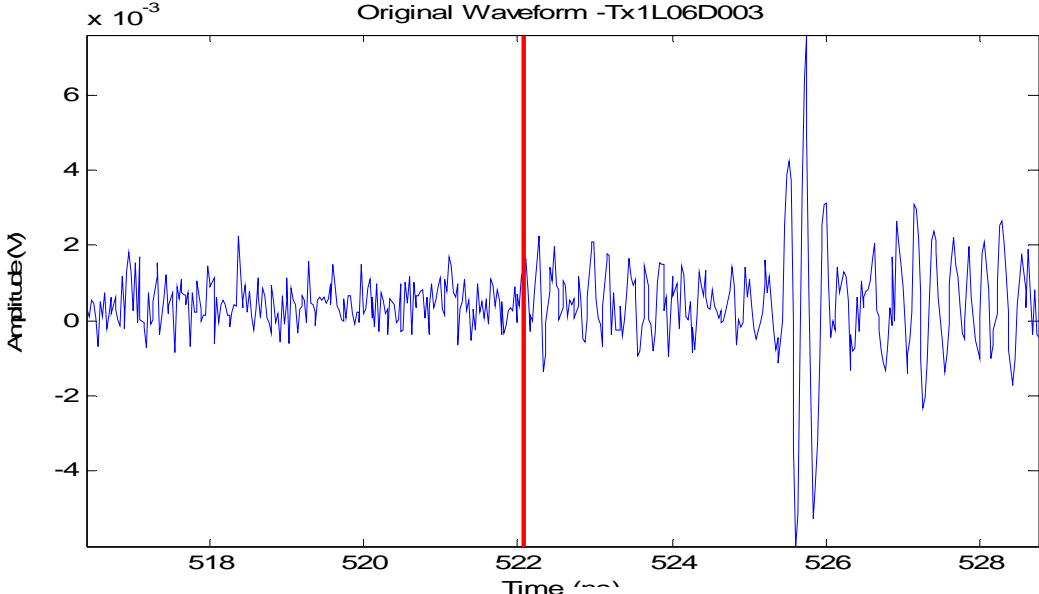
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# Received direct path pulse shape with Tx-Rx distance of 1m



# NLOS received waveforms with heavy blockage



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# Ranging Algorithm Problem Statement

- Time of Arrival ranging systems using impulse radio UWB
- What is the optimum threshold setting and search window size for direct path detection
- How does SNR, LOS and NLOS environments affect these optimum settings

# Ranging Performance Analysis

The received signal  $r(t)$  is modeled as,

$$r(t) = \alpha_d s(t - \tau_d) + \sum_{i=1}^L p_i \alpha_i s(t - \tau_i) + n(t) \quad \dots\dots\dots \text{Eq (1)}$$

Where  $\alpha_d$  and  $\tau_d$  are the amplitude and propagation delay of direct path

$\alpha_i$  and  $\tau_i$  are the amplitude and propagation delay of  $i^{\text{th}}$  multipath

$p_i$  is the polarity of  $i^{\text{th}}$  multipath

$n(t)$  is the WGN process

After correlated with the pulse template, the resulting waveform within  $[\tau_p - \delta, \tau_p]$  can be expressed

$$R_c(t) = \alpha_d R_{ss}(t - \tau_d) + \sum_{i=1}^M p_i \alpha_i R_{ss}(t - \tau_i) + R_{ns}(t) \dots \dots \dots \text{Eq (2)}$$

Where  $R_{ss}$  is the autocorrelation function of pulse template

$$\alpha_M = \alpha_p \text{ and } \tau_M = \tau_p$$

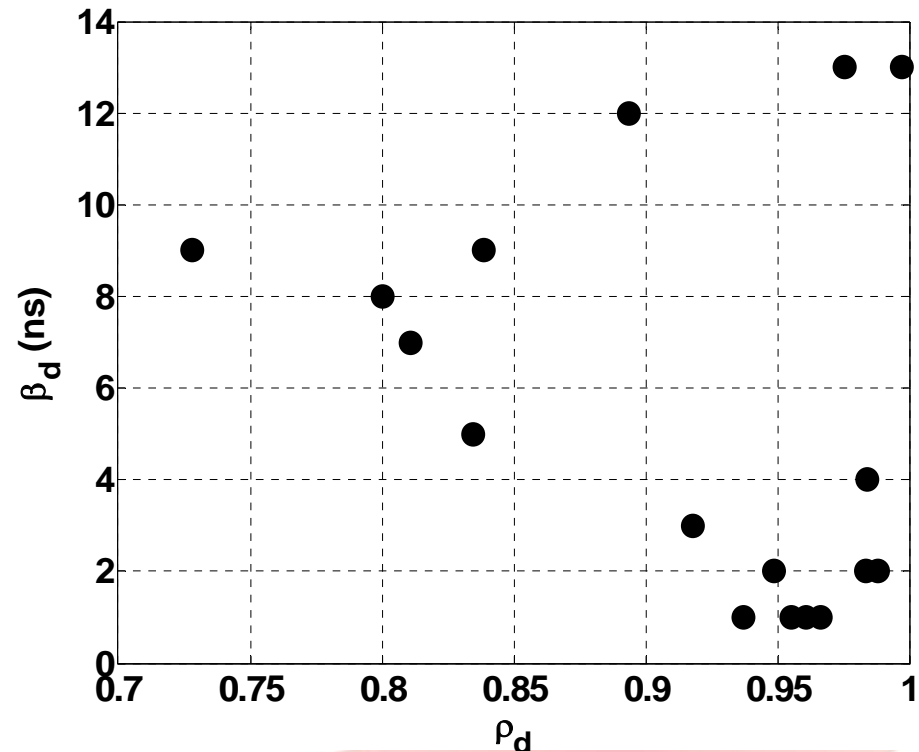
Let us define:  $\rho_d = \alpha_d / \alpha_p$  (Normalized direct path amplitude)

$\beta_d = \tau_p - \tau_d$  (Time difference between Peak path and Direct path)

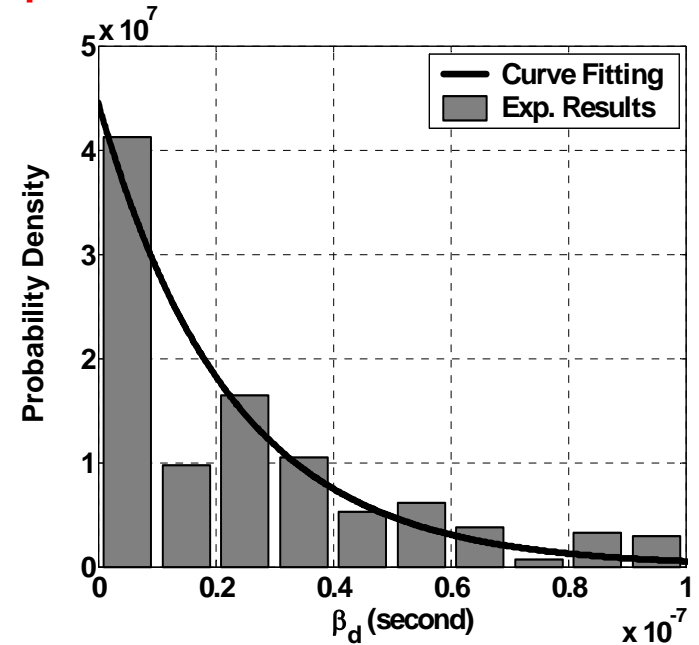
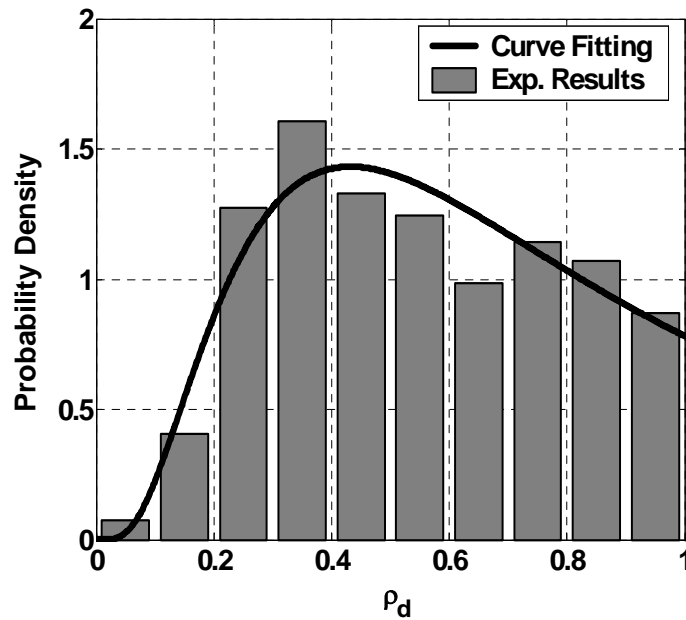


# Conclusion on Ranging settings for LOS

- According to measurement results, the direct path is not the largest path in 17 profiles out of 289 profiles in LOS.
- For LOS, simple strategy is enough:  
setting search period  $\delta > 20ns$  and detection threshold  $\gamma = m \alpha_p$  with  $m=0.5\sim 0.6$



# Distribution of NLOS Direct Path Amplitude and Time of Arrival



$$f_{\rho_d}(\rho_d | \rho_d \neq 1) = \frac{1}{\sqrt{2\pi}Q(-\mu/\sigma_\rho)\sigma_\rho\rho_d} \exp\left[-\frac{((\ln \rho_d) - \mu)^2}{2\sigma_\rho^2}\right] \dots\dots \text{Eq (3)}$$

where  $Q(x) = \int_{-\infty}^x \frac{1}{\sqrt{2\pi}} \exp\left[-\frac{x^2}{2}\right] dx$  ;  $f_{\beta_d}(\beta_d | \beta_d \neq 0) = \frac{\beta_d}{\eta} \exp\left[-\frac{\beta_d}{\eta}\right]$

..... Eq (4)

- Evaluate the performance by large error probability  
(  $|\text{Estimated arrival time of direct path} - \text{true arrival time of direct path}| > T_c/2$ )
- The large error probability is related to three events

$$H_1 = \{\beta_d > \delta\}$$

$$H_2 = \{\beta_d \leq \delta\} \cap \{|\alpha_d + n_{ns}| < \gamma\}$$

$$H_3 = \{Z_{\max} > \gamma\} \cap \{|\alpha_d + n_{ns}| \geq \gamma\}$$

Where,  $Z_{\max} = \sup\{|R_{ns}(t)|\}$  ,  $t \in [\tau p - \delta, \tau p]$  and  $\delta \geq \beta_d$ .

$$n_{ns} = R_{ns}(\tau p),$$

- Since three events are exclusive, the large error probability is

$$P_{Lgr}(\gamma, \delta) = P(H_1) + P(H_2) + P(H_3) \dots\dots\dots \text{Eq (5)}$$

Ignoring the intermediate derivation process , the final equation will be,

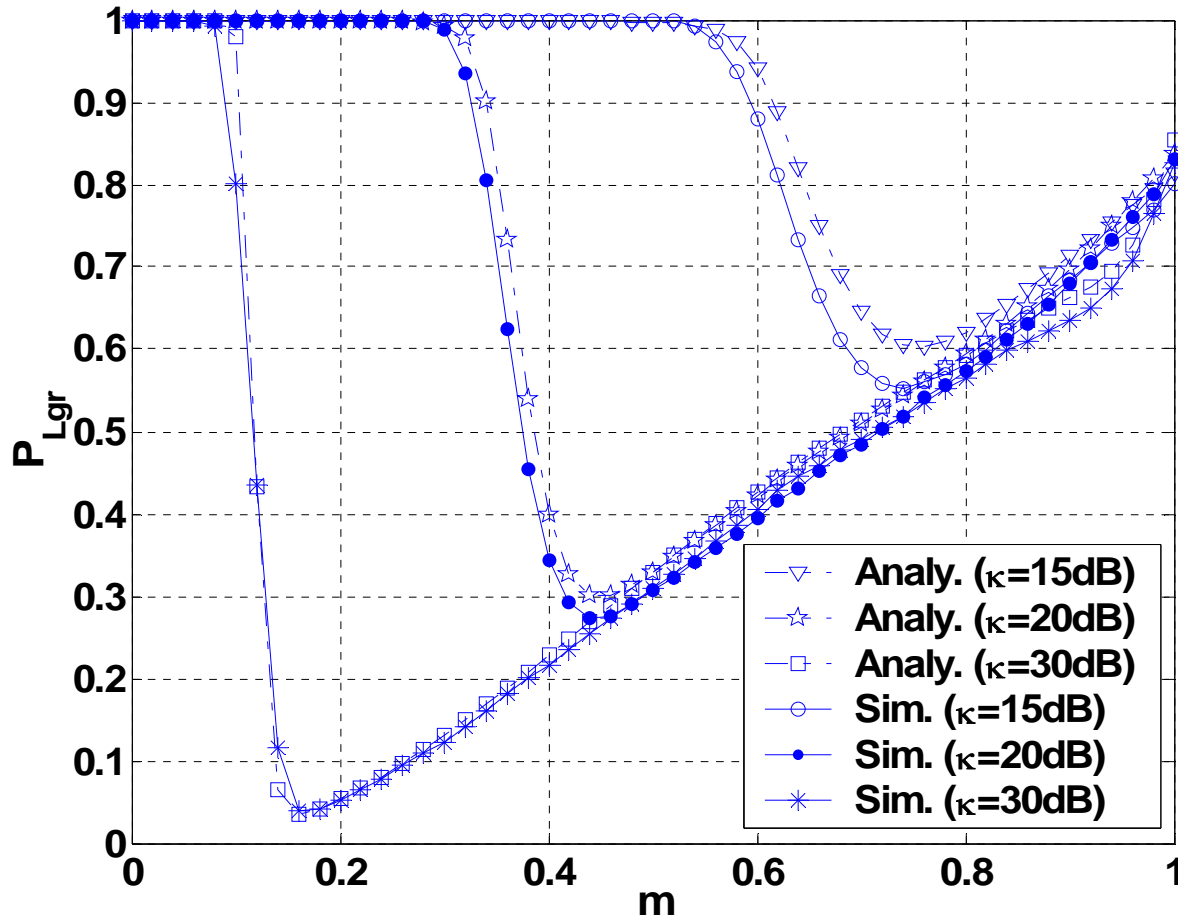
$$P_{Lgr} = 1 - P_0 \exp\left[-\frac{\delta}{\eta}\right] \left(1 - \Psi(m, \kappa)\right) + \left(1 - (1 - P_0)\Gamma(m, \kappa) - P_0\Psi(m, \kappa)\right)$$

$$\bullet \left( \exp\left[-\frac{\delta}{\eta}\right] - \exp\left[-\frac{2\delta}{\Omega(m, \kappa)}\right] \right) \left( \frac{2\eta P_0 - \Omega(m, \kappa)}{2\eta - \Omega(m, \kappa)} \right) \dots\dots\dots Eq (6)$$

Where  $m = \frac{\gamma}{\alpha_p}$  is normalized threshold

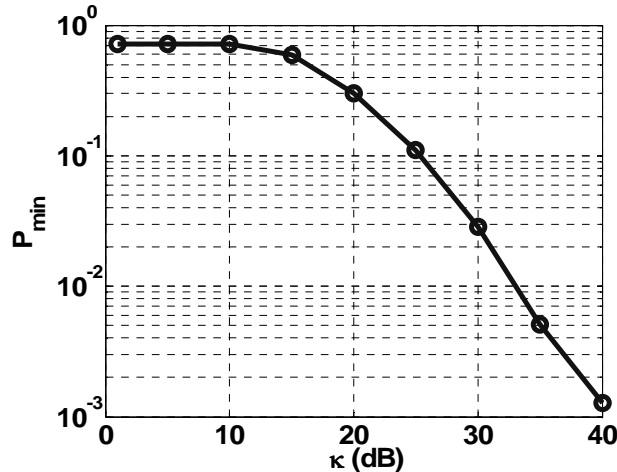
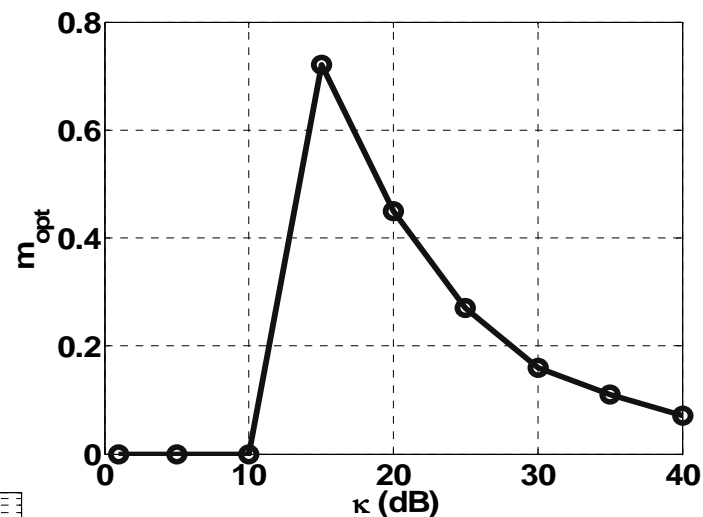
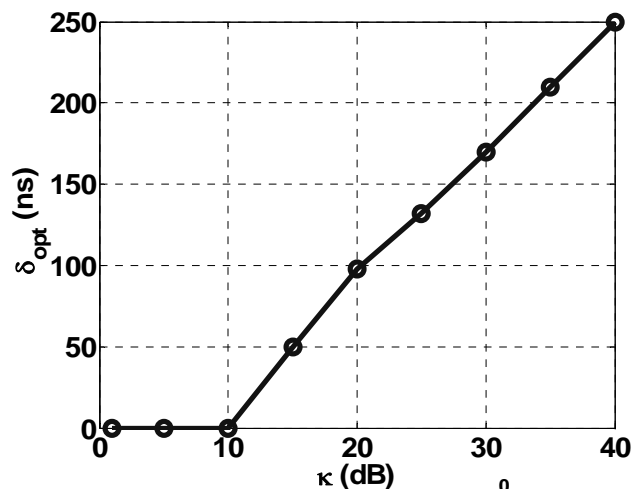
$\kappa = \frac{\alpha_p}{\sigma_{ns}}$  is signal-to-noise (SNR) ratio

# Comparison of simulation and analytical results, (Search window size=100nS)

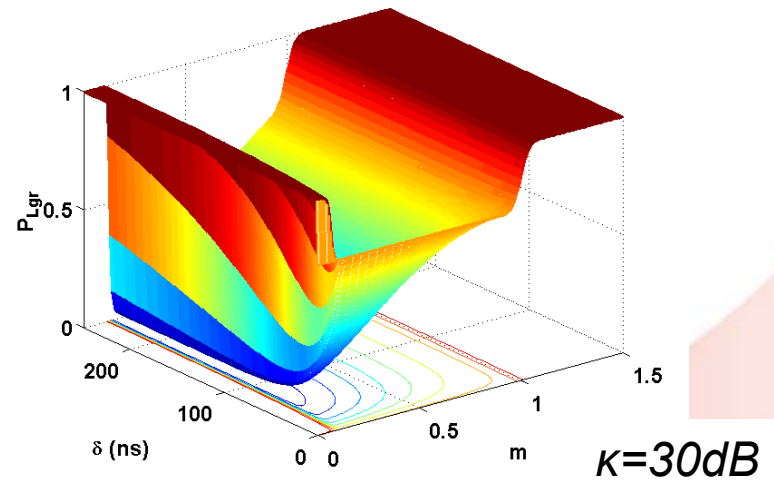
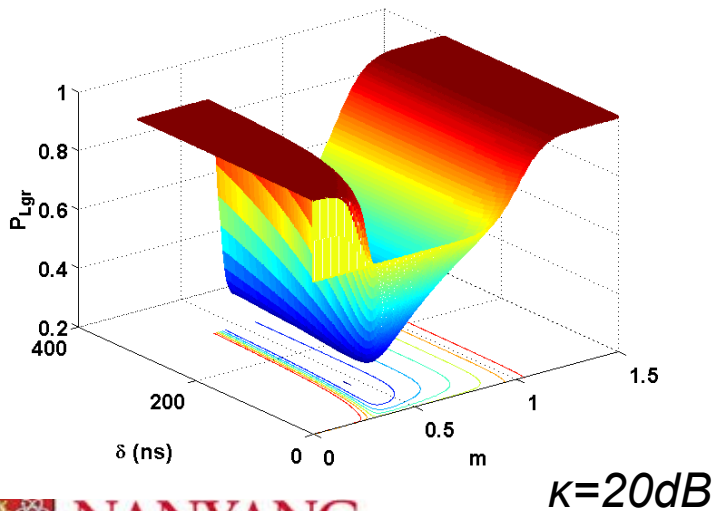
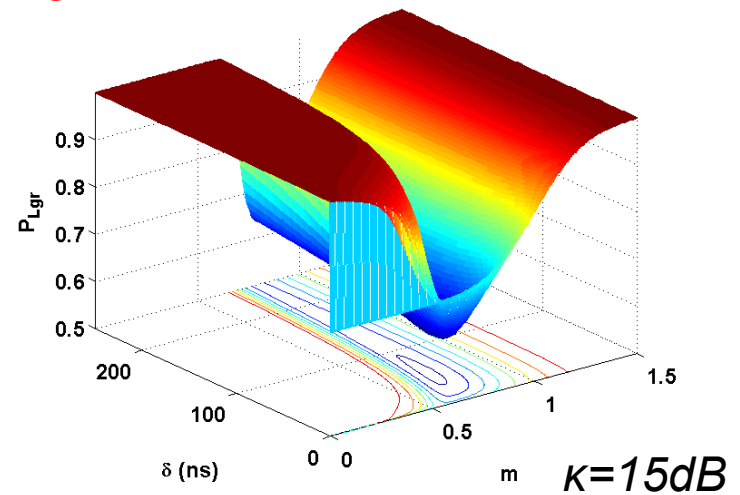
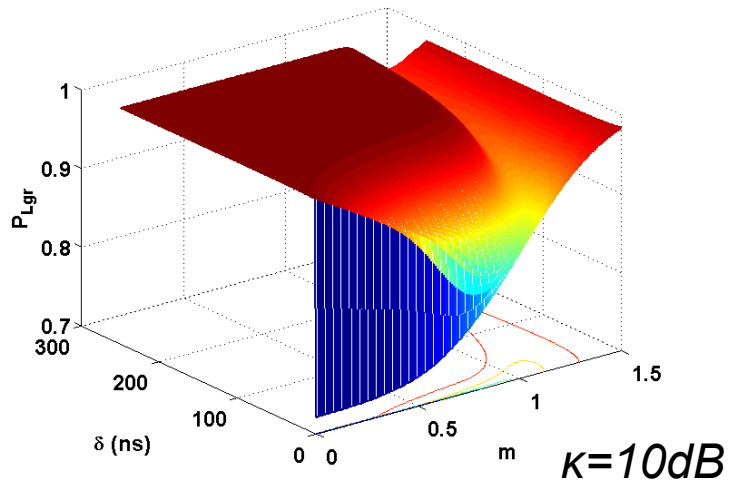


# Adaptive ranging parameters Setting

For NLOS, if channel parameters are given, numerical search may be performed with  $Eq(6)$  to obtain the optimum setting



# Performance curves for various SNR and search windows size



## Conclusion on Ranging settings for NLOS

For NLOS, If channel parameters are not available, a two-state threshold settings method is proposed:

(1).  $\delta$  is predefined and fixed. A worst-case false alarm rate  $P_{fls}$  is predefined

$$m = \frac{1}{\kappa} \sqrt{2 \ln \left( \frac{-\delta \lambda_0}{\ln(1 - P_{fls})} \right)}$$

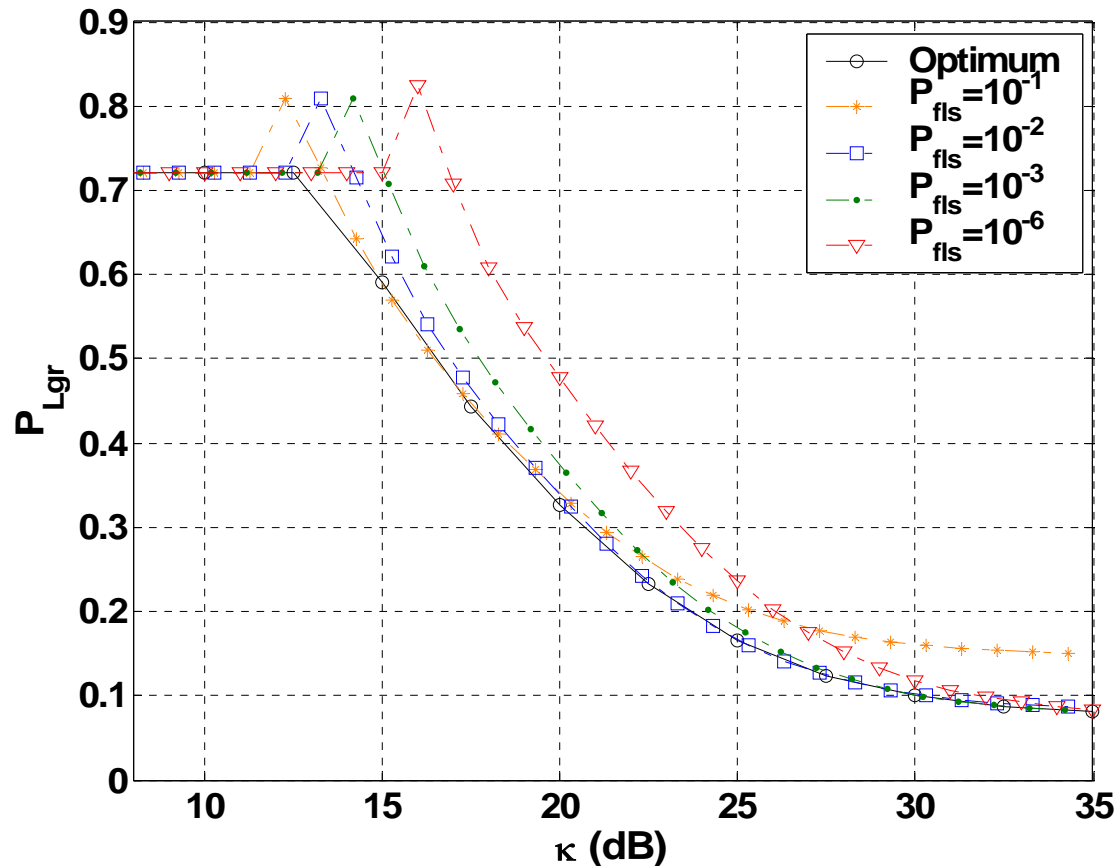
$\lambda_0$  is a parameter related to the RMS bandwidth of pulse template

(2). If the calculated  $m$  for a particular  $\kappa$  is larger than 1, the largest path is taken as the direct path and the earliest path searching path does not initialize.





# Performance of optimum setting by numerical searching versus performance of two-state setting strategy with $\delta = 50\text{ns}$

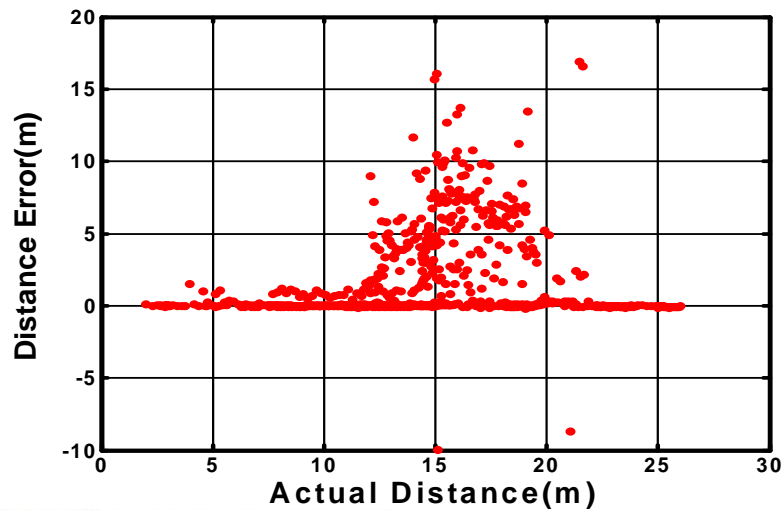
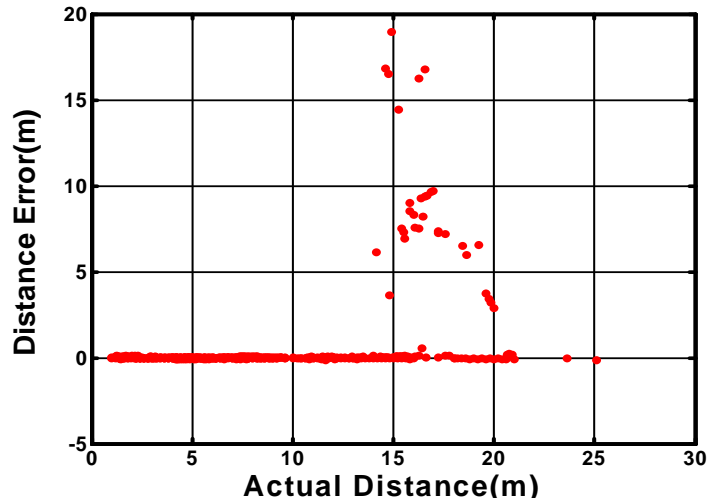


# Ranging Error Performance

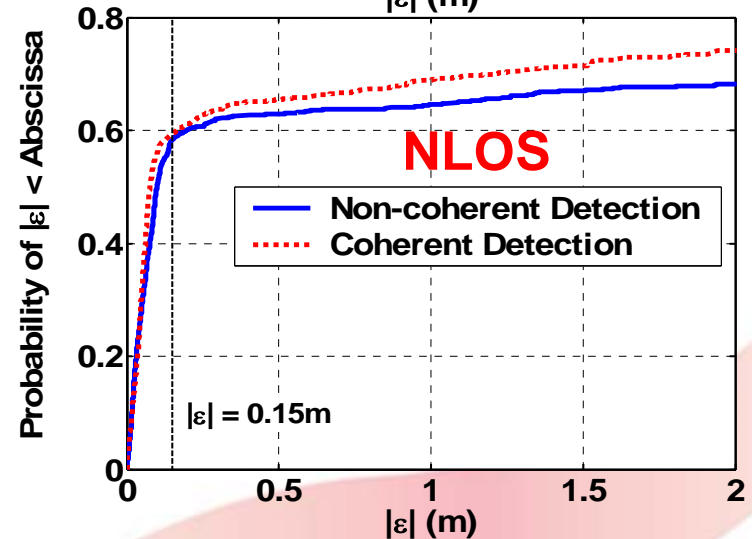
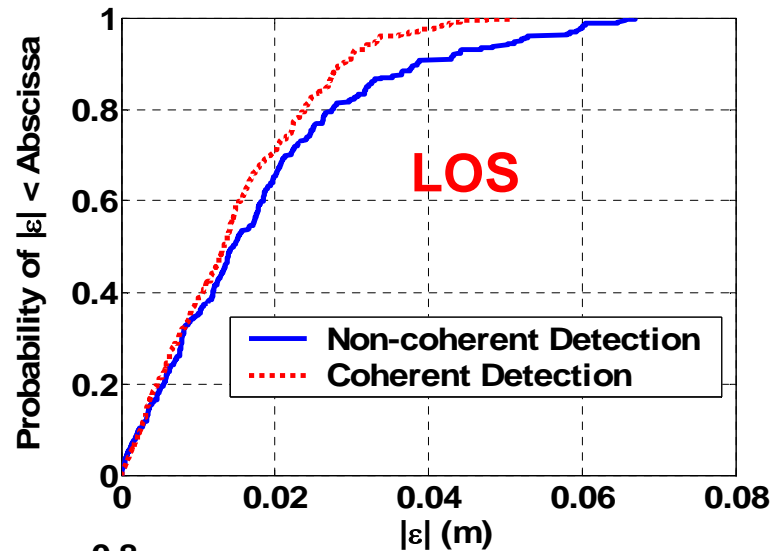
- Comparison of Coherent (CLEAN) and Non-coherent (Energy detection)

|                                  | Indoor Office |        | Lab   | Open Hall | Corridor |
|----------------------------------|---------------|--------|-------|-----------|----------|
|                                  | LOS           | NLOS   |       |           |          |
| <b>By Non-Coherent Detection</b> |               |        |       |           |          |
| Mean (m)                         | 0.018         | 4.336  | 0.011 | 0.031     | 0.020    |
| STD. (m)                         | 0.015         | 10.220 | 0.014 | 0.019     | 0.015    |
| Max (m)                          | 0.067         | 93.094 | 0.077 | 0.080     | 0.056    |
| <b>By Coherent Detection</b>     |               |        |       |           |          |
| Mean (m)                         | 0.015         | 2.004  | 0.010 | 0.015     | 0.011    |
| STD. (m)                         | 0.010         | 3.784  | 0.013 | 0.012     | 0.008    |
| Max (m)                          | 0.051         | 38.505 | 0.080 | 0.049     | 0.031    |

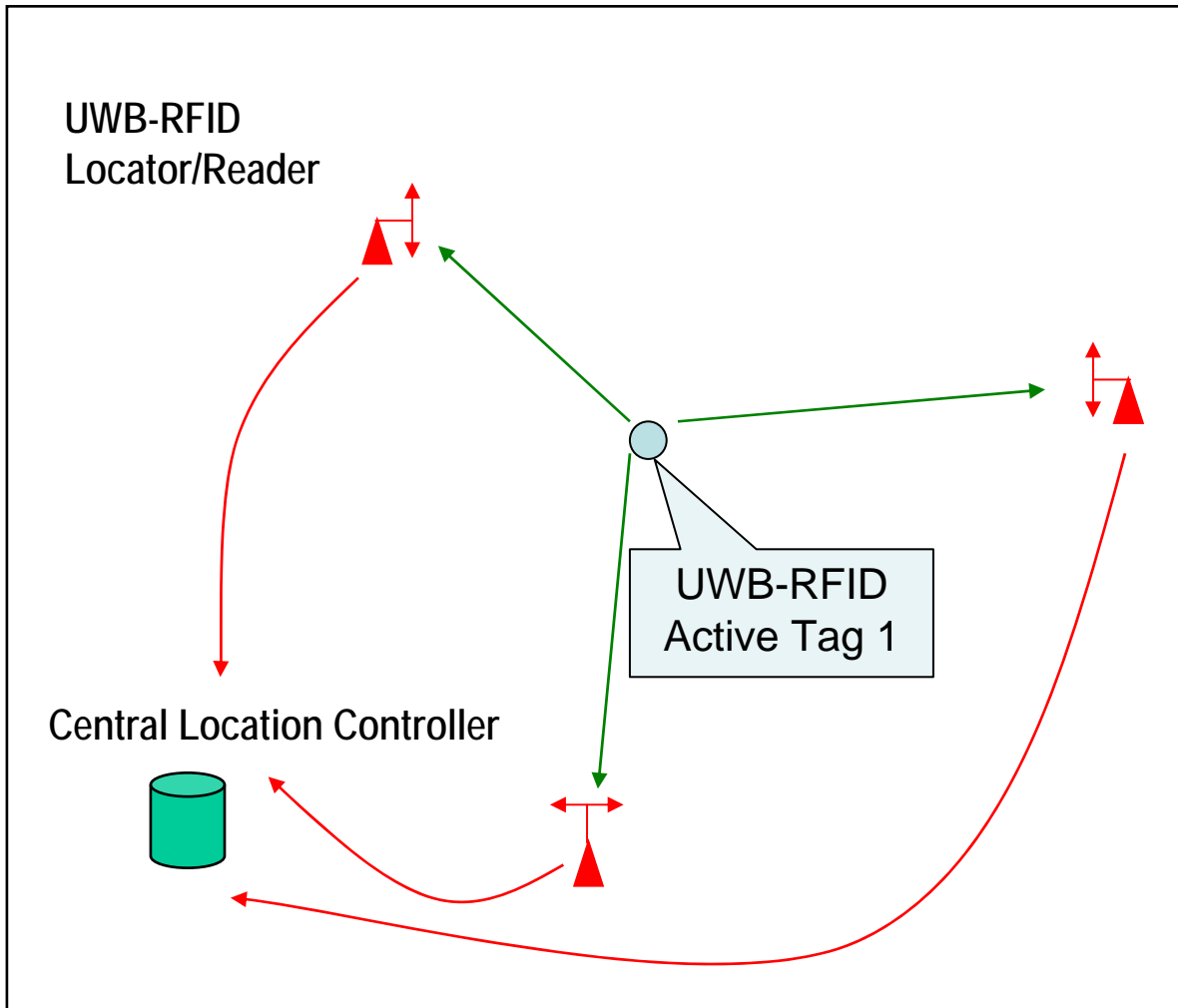
# Ranging Error Performance



- CDF of ranging errors  $|\varepsilon|$



# Active UWB-RFID Localization

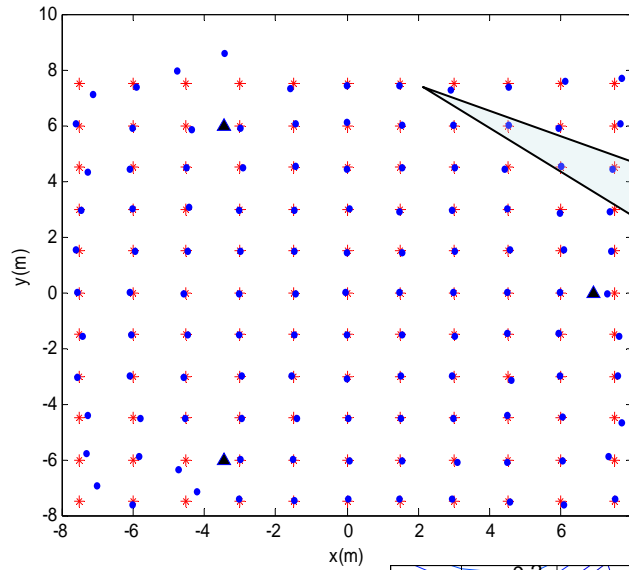
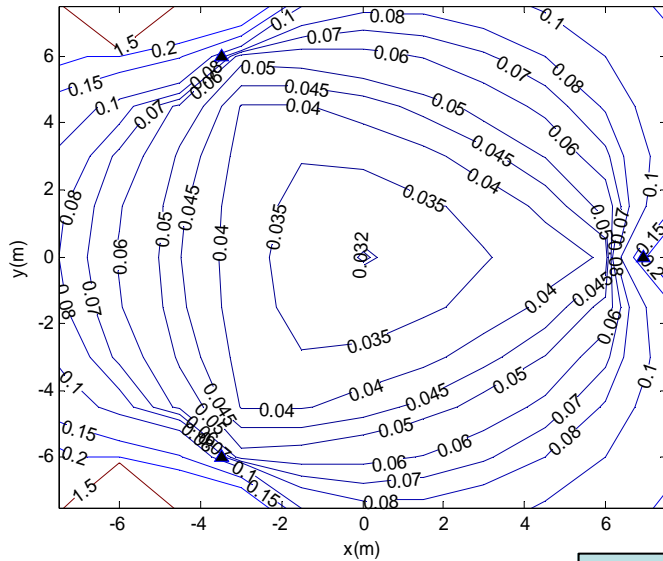


## Active UWB-RFID:

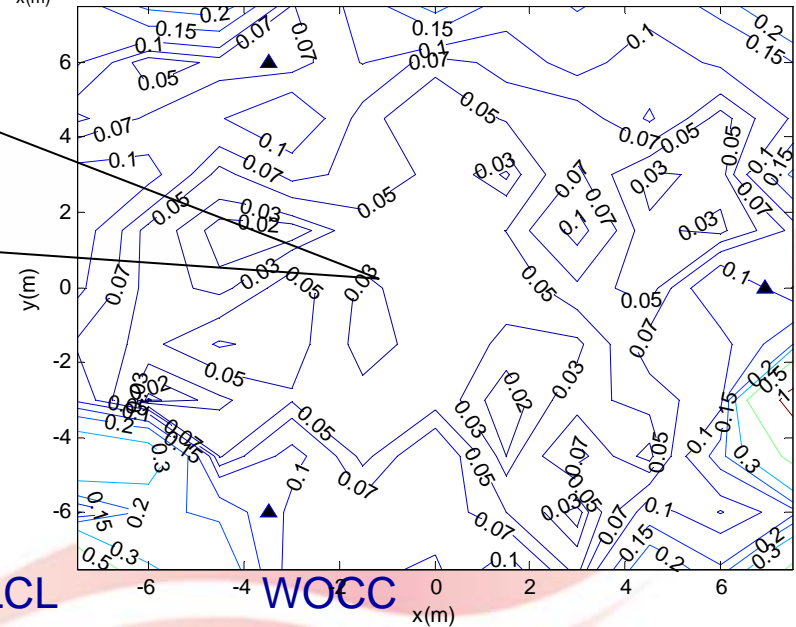
- TDOA computation in central controller
- Time synchronization among locators are through a hard wire

# Active UWB-RFID Localization using TDOA

## Lower bound of positioning error



Positioning error between UWB measured locations and actual locations of 121 points. Most locations positioning error < 10cm



**End of Presentation**

**Thank you for your attendance**



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- (v) Mr Zhou Yuan – Full time PhD student (AGS scholar)
- (vi) Ms Jiang Jisu – Full time PhD student
- (vii) Ms Thida Than – Research Engineer



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